The Effect of Copper and Brass on Friction Stir Welded Dissimilar Aluminium Alloy When Used as in Thin Sheet Form

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Abstract: In recent year's aluminium and aluminium alloys are most widely used in many applications because of light weight, good formability and malleability, corrosion resistance, moderate strength and low cost. Friction Stir Welding (FSW) process is efficient and cost effective method for welding aluminium and aluminium alloys. FSW is a solid state welding process that means the material is not melted during the process. Complete welding process accomplishes below the melting point of materials so it overcomes many welding defects that usually happens with conventional fusion welding technique which were initially used for low melting materials. Though this process is initially developed for low melting materials but now process is widely used for a variety of other materials including titanium, steel and also for composites. The present butt jointed FSW experimental work has been done in two ways. Initially a comparison of tensile properties of friction stir (FS) welded similar aluminium alloy (AA6351 with AA6351) and dissimilar aluminium alloy (AA6351 with AA5083) combinations. Later the effect of impurities (copper and brass) in sheet form (0.1 mm thick) when used as insert in between two dissimilar aluminium alloy (AA6351 with AA5083) plates during FSW. Tensile tests were performed for these combinations and results were compared for with and without using strip material (copper and brass).

Keywords: Friction Stir Welding, Tensile behaviour, Aluminium alloys AA6351 and AA5083, Copper and Brass.

INTRODUCTION

Friction Stir Welding (FSW) is a new solid state welding process (means material is not melted during the welding process) which is developed and patented by The Welding Institute (TWI) in 1991. This process found world wide acceptance throughout the joining and welding community since its inception and emerged as a novel welding technique to be used for high strength alloys that were difficult to join with conventional fusion welding techniques¹. Though this process initially developed for aluminium alloys²⁻¹⁰, but latter FSW has been found suitable for joining of a variety of other materials like magnesium^{11, 12}, steel¹³, ¹⁴, titanium¹⁵, copper^{16, 17} and also for composites¹⁸.

The basic principle of FSW process is simple. Instead of a conventional welding torch, friction stir welding uses a non consumable rotating tool (harder than material to be welded) with a specially designed shoulder and pin is inserted into the abutting edged of the two parts to be welded and traversed along the line of the joint as shown in Fig.1. The heating is localised and generated by friction between the rotating tool and workpiece, with additional adiabatic heating from metal deformation. The shoulder and pin of the tool can be modified in number of ways to influence material flow and microstructural formation.

Mechanical properties can improve by various techniques in FSW process such as post weld heat treatment^{19, 20}, pre heating the weld during the process²¹, different types of peening processes²² and overlapping weld passes²³. Though FSW process requires no additional material during the process but alloying elements addition of influences microstructure and improves mechanical properties in aluminium alloys²⁴. So, an effort has been made to improve the mechanical properties by adding copper and brass (an alloy of copper and zinc) separately to dissimilar aluminium alloy combination, in thin sheet form during FSW.

EXPERIMENTAL PROCEDURE

Aluminium AA6351(standard and experimental chemical compostion shown in Table 1) and AA5083 (standard and experimental chemical compostion shown in Table 2) alloys of 5 mm thickness plates were friction stir (FS) welded in butt joint configuration. Both alloys were FS welded with different combination. Initially similar aluminium combination, AA6351 alloy with AA6351 alloy and dissimilar aluminum combination, AA6351 with AA5083 alloy were FS welded as shown in Fig.2. Later dissimilar aluminium alloy combination were FS welded separately with copper (99.95 % of copper) and brass (65 % of copper and 35 % of zinc) sheets of thickness 0.1 mm used as inserts in between two dissimilar aluminium alloy (AA6351 with AA5083) plates separately as shown in Fig.3.



Figure1. Friction Stir Welding (FSW) Process.

Table I. Standard chemical composition and chemical
composition of base material (Aluminium alloy
AA6351) used for experiments

		Base material
Element	Standard	used for
		experiments
Si	0.8	0.7
Fe	0.5	0.357
Cu	0.1	0.037
Mn	0.4	0.35
Mg	0.4	0.3
Zn	0.2 max	0.004
Ti	0.2 max	0.024
Al	Balance	Balance

Table 2. Standard chemical composition and chemical composition of base material (Aluminium alloy AA5083) used for experiments

Element Standard used for experiments	Element	Standard	Base material used for experiments
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Si	0.2	0.134
Fe	0.35	0.284
Cu	0.15	0.028
Mn	0.15	0.58
Mg	5	4.466
Zn	0.25	0.006
Ti	0.1	0.021
Al	Balance	Balance

Figure 2. Process FSW of AA6351 with AA6351	and
AA6351 with AA5083.	

The tool material used in this work was high speed steel (HSS) with conical shape probe without threads. Then the tool was subjected to heat treatment to improve hardness, the hardness tool after the heat treatment process is 54 HRC.

A vertical Compter Numerically Controlled (CNC) milling machine was used to carry out welding process. The two plates are partitioned in the fixture which is prepared for fabricating FSW joint by using mechanical clamps so that the plates will not separate during the welding process. Two aluminium alloys were perfectly clamped in CNC milling machine bed on a back plate. Tool is plunged into the joint in the downward direction. Higher tool rotation generates temperature because of higher frictional heating and



resulted more intense stirring of mixing material.

Figure 3. Process FSW of AA6351 with AA5083 with copper/brass thin sheet.

Journal of Mechanical Engineering, Vol. ME 45, No. 2, December 2015 Transaction of the Mechanical Engineering Division, The Institution of Engineers, Bangladesh

RESULTS AND DISCUSSIONS

Tensile tests were performed to determine the tensile properties (yield strength, tensile strength and percentage elongation) for all FS welded all combination samples. Tensile properties were lower at lower rotational speeds of the tool and increases with increase in rotational speeds and after reaching optimum value reverse trend has been observed i.e., tensile properties decrease with increase in rotational speed of the tool. This type of trend observed for all the combinations of alloys i.e., similar alloy, dissimilar alloy and dissimilar alloy using strip material combinations.

Figures 4,5 and 6 shows the effect of rotational speed of the tool on yield strength, tensile strength and percentage elongation of similar aluminium alloy combination, AA6351 alloy with AA6351 alloy and dissimilar aluminum alloy combination, AA6351 alloy with AA5083 alloy respectively. It is clear from these figures that at lower rotaional speed (1000 rpm), tensile properties of both similar and dissimilar alloy combination were lower and reaches maximum at 1300 rpm. After reaching optimum value at 1300 rpm rotaional speed, tensile properties decreases with increase in rotaional speed of the tool. This type of trend coincided with authers²⁵²⁶.

Lower rotational speeds of the tool, lowers the heat input during FSW which results lower tensile properties because of wavy zigzag pattern formation on weldment cross section²⁷ and crack or pinhole defect²⁵. Higher rotational speed of the tool results higher temperature at weld joint²⁸ which results large size defect like tunnel²⁵

Similar aluminium alloy combination AA6351 with AA6351 shows higher tensile properties compared to dissimilar alloy combination AA6351 with AA5083 because weaker alloy (AA5083) dictates the performace of the weld joint²⁹



Figure 4. Effect of rotational speed of tool on yield strength for both similar and dissimilar aluminium alloy combination.



Figure 5. Effect of rotational speed of tool on tensile strength for both similar and dissimilar aluminium alloy combination.





Figures 7. 8 and 9 shows the effect of rotational speed of the tool on yield strength, tensile strength and percentage elongation of dissimilar aluminum combination AA6351 with AA5083 alloy, dissimilar AA6351, AA5083 with copper and brass strip material respectively. It is clear from these figures that at lower rotational speed (1000 rpm), tensile properties of all the combination were lower and reaches maximum at 1300 rpm. After reaching optimum value at 1300 rpm rotaional speed, tensile properties decreases with increase in rotaional speed of the tool. Tensile values of dissimilar alloy combination with copper addition values are lower than pure dissimilar combination. Tensile values of dissimilar alloy combination with brass additon values lower than both pure dissimilar combination and also copper additon combination. The main reason of lower values for copper and brass addition are complete melting of copper and brass material was not taking place at bottom sides of the welded plates though sheet thickness of copper and brass is too small (0.1mm).



Figure 7. Effect of rotational speed of tool on yield strength for pure dissimilar aluminium alloy, and the effect of copper and brass addition on dissimilar aluminium alloy combinations.



Figure 8. Effect of rotational speed of tool on tensile strength for pure dissimilar aluminium alloy, and the effect of copper and brass addition on dissimilar aluminium alloy combinations.



Figure 9. Effect of rotational speed of tool on percentage elongation for pure dissimilar aluminium alloy, and the effect of copper and brass addition on dissimilar aluminium alloy combinations.

CONCLUSIONS

The following conclusions are arrived from the present work.

• Tensile values (yield strength, tensile strength and percentage elongation) are lower at lower rotational speed of the tool, increases with increase

in rotational speeds and reaches optimum at a particular value of speed (1300 rpm) and thereafter, values came down with increase in rotational speed of the tool. This trend is common for all types of combinations.

- Tensile values of similar aluminium alloy combination of AA6351 with AA6351 are greater than the dissimilar aluminium alloy combination of AA6351 with AA5083.
- Tensile values of copper addition with dissimilar aluminium alloy combination of AA6351 with AA5083 are lower than pure dissimilar aluminium alloy combination of AA6351 with AA5083 but better than that of brass addition with dissimilar aluminium alloy combination of AA6351 with AA5083.

REFERENCES

1. W. Thomas, E. Nicholas, J. Needham, M. Murch, P. Templesmith, C. Dawes, 1995, Patent-Friction stir butt welding, I.P.N.PCT/GB92/02203, Editor, GB Patent No. 9125978.8, US Patent No.5.460.317. (1991).

2. Yeong-Maw Hwang , Zong-Wei Kang , Yuang – Cherng Chiou , Hung – Hsiou Hsu, Experimental study on temperature distributions within the workpiece during friction stir welding of aluminium alloys, International journal of machine tools & manufacture, 48 (2008), pp.778-787.

3. Hua-Bin Chen, Keng Yan, Tao Lin, Shan-Ben Chen, Cheng-Yu Jiang, Yong Zhao, The investigation of typical welding defects for 5456 aluminium alloy friction stir welds, Material science and engineering A, 433 (2006), pp. 64-69.

4. K. Elangovan, V. Balasubramanian, Influences of post weld heat treatment on tensile properties of friction stir-welded AA6061 aluminium alloy joints, Material charichtacterization 59 (2008), pp.1168-1177.

5. P.M.G.P. Moreira, T. Santos, S.M.O. Tavares, V. Richter-Trummer, P. Vilaca, P.M.S.T.de Castro, Mechanical and metallurgical characterization of friction stir welding joints of AA6061-T6 with AA6082-T6, Materials and design, 30 (2009), pp. 180-187.

6. C. Leitao, R.M.Leal, D.M. Rodrigues, A. Loureiro, P. Vilaca, Mechanical behaviour of similar and dissimilar AA5182-H111 and AA6016-T4 thin friction stir welds, Materials and design, 30 (2009), pp. 101-108.

7. W. Gan, K. Okamoto, S. Hirano, K. Chung, C. Kim, R.H. Wagoner, Properties of friction-stir welded aluminium alloys 6111 and 5083, Journal of engineering materials and technology, 130 (2008), pp. 031007-1 – 031007-15.

Journal of Mechanical Engineering, Vol. ME 45, No. 2, December 2015 Transaction of the Mechanical Engineering Division, The Institution of Engineers, Bangladesh 8. W.B. Lee, Y.M. Yeon, S.B. Jung, The improvement of mechanical properties of friction-stir-welded A356 Al alloy, Material science and engineering A, 355 (2003), pp.154-159.

9. Yutuka S. Sato, Hideki Takauchi, Seung Hwan C. Park, Hiroyuka Kokawa, Characteristics of the kissing-bond in friction stir welded Al alloy 1050, Material science and engineering A, 405 (2005), pp. 333-338.

10. William D. Lockwood, Borislav d, A.P. Reynolds, Mechanical response of friction stir welded AA2024: experiment and modelling, Material science and engineering A, 323 (2002), pp. 348-353.

11. Dr. Richard Johnson, Dr. Philip Threaddill, Friction stir welding of magnesium alloys, Magnesium technology 2003, Edited by Howard I. Kaplan TMS (The minerals, metals & material society), (2003), pp.147-152.

12. Naiyi, Li, Tsung-Yu Pan, Ronald P.Cooper, Dan Q. Houston, Zhili Feng and L. Santella, Friction stir welding of magnesium AM60 alloy, Magnesium technology 2004, Edited by Alan A. Luo TMS (The minerals, metals & material society), (2004), pp.19-23 13. T.J. Lienert, W.L. Stellwag, JR., B.B. Grimmett, and R.W. Warke, Friction stir welding studies on mild steel, Welding research, Supplement to the welding journal (January 2003), pp.1s-9s.

14. Ling Cui, Hidetoshi Fujii, Nobuhiro Tsuji and Kiyoshi, Nogi, Friction stir welding of a high carbon steel, Scripta Materialia, 56 (2007), pp. 637,640.

15. Yu Zhang, Yutaka S. Sato, Hiroyuki Kokawa , Seung Hwan C. Park ,Satoshi Hirano , Microstructural characteristics and mechanical properties of Ti-6Al-4V friction stir welds, Material science and engineering A, 485 (2008), pp. 448-455.

16. Z. Barlas, H.Uzum, Microstructure and mechanical properties of friction stir butt welded dissimilar Cu/CuZn30 sheets, Journal of achievements in materials and manufacturing engineering, 30(2) (2008), pp.182-186.

17. Ratnesh K.Shukla, Dr. Pravin K. Shah, Experimental investigations of copper joining by friction stir welding, proceedings of the international conference on emerging research and advances in mechanical engineering (ERA 2009), Velammal engineering college, Chennai-600 066, Taminadu, India. Pp.657-660

18. L. Ceschini, I. Boromei, G. Minak, A. Morri, F. Tarterini, Effect of friction stir welding on microstructure, tensile and fatigue properties of the AA7005/10 vol.%Al₂O_{3p} composite, Composites science and technology, 67 (2007), pp. 605-615.

19. K.Elongovan, V.Balasubramanian, Influences of post weld heat treatment on tensile properties of friction stir welded AA6061 aluminium alloy joints, Materials Characterization (2008), vol. 59, pp. 1168-1177.

20. G. Madhusudhan Reddy, P. Mastanaiah, C.V.S. Murthy, T. Mohandas and N. Viswanathan, Microstructure, residual stress, distribution and mechanical properties of friction stir AA60611 aluminium alloy weldments, Proc. National Seminar on Non-Destructive Evaluation (Dec. 7-9, 2006) Hyderabad.

21. Omid Ali Zargar, The preheating influence on welded joint mechanical properties prepared by friction stir welding aluminium alloy H20-H20, Middle East Journal o Scientific Research (2013), Vol. 15, pp. 1415-1419.

22. Omar Hatamleh, Effect of peening on mechanical properties in friction stir welded 2195 aluminum alloy joints, Materials Science and Engineering A (2008), vol. 492, pp. 168-176.

23. R.M.Leal and A.Loureiroir, Effect of overlapping friction stir welding passes in the quality of welds of aluminium alloys, Materials and Design (2008), vol. 29, pp. 982-991.

24. R.S.Rana, Rajesh Purohith and S.Das, Reviews on the influences of alloying elements on the microstructure and mechanical properties of aluminium alloys and aluminium alloy composites, International Journal of Scientific and Research Publications (2012), vol. 2, pp. 1-7.

25. K. Elagovan, V. Balasubramanian, S. Balu, Predicting tensile strength of friction stir welded AA6061 aluminium alloy joints by a mathematical model, Materials and Design (2009), vol. 30, pp. 188-193.

26. R.Palanivel, P.Koshy Mathews and N.Murugan, Development of mathematical model to predict the mechanical properties of friction stir welded AA6351 aluminium alloy, Journal of Engineering Science and Technology Review (2011), vol. 4, pp. 25-31.

27. Yutako S.Sato, Hideaki Takauchi, Seung Hwan C.Park, Hiroyuki Kokawa, Characteristics of the kissing bond in friction stir welded Al alloy 1050, Materials Science and Engineering A (2005), vol. 405, pp. 333-338.

28. Weifeng Xu, Jinhe Liu, Guohong Luan, Chunlin Dong, temperature evolution, microstructure and mechanical properties of friction stir welded thick 2219-O aluminium alloy joints, Materials and Design (2009), vol. 30, pp. 1886-1893.

29. S.T.Amancio-Filho, S.Sheikhi, J.F.dos Santos, C.Bolfarini, Preliminary study on the microstructure and mechanical properties of dissimilar friction stir welds in aircraft aluminium alloys 2024-T351 and 6056-T4, Journal of Materials Processing Technology (2008), vol. 206, pp. 132-142.