

Assessing the Treatment Efficiency of a Multi-Stage ETP for Pharmaceutical Wastewater: A Case Study in Bangladesh

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Effluent; Reed Bed.

Abstract

This study assessed the treatment efficiency of the physical, chemical, and biological treatment processes to treat effluent discharged for a pharmaceutical factory. The treatment mechanism comprised of equalization tank, neutralization tank, anaerobic followed by aerobic bioreactors, two stage clarification system, reed bed bio-filtration process, and post aeration system. The effluent quality parameters such as pH, turbidity, TDS, TSS, TS, COD and BOD₅ were analyzed in the laboratory with standard methods. The overall pollution removal efficiencies were 100% for turbidity, 97% for TSS, 95% for COD, and 97% for BOD₅. The average reduction ranges of Turbidity, TSS, TS, COD and BOD₅ were 201 FTU to 0 FTU, 512 mg/l to 13 mg/l, 912 mg/l to 530 mg/l, 2034 mg/l to 99 mg/l, and 1126 mg/l to 29 mg/l respectively were observed in the final stage. In terms of performance evaluation of individual treatment units, the anaerobic treatment unit achieved 1%, 17%, and 37% removal efficiencies for turbidity, COD, and BOD₅ respectively; while the aerobic unit achieved 76%, 86%, and 86% removal efficiencies for the same parameters. The chemical treatment process was found effective for TSS and turbidity removal purpose. The Reed Bed performed well in removing BOD₅, COD, and Turbidity.

1. Introduction

The pharmaceutical industries which play a vital role in global health sector but generates complex and diverse toxic wastewater to the streams as well. Such toxic substances induce significant environmental and public health challenges. The pharmaceutical effluents have versatile chemical compositions which create high chemical and biochemical oxygen requirements and contain some residual pharmaceutical substances. Strong treatment strategies are essential to mitigate the biotoxicity, toxicity, and persistence of these substances. The conventional wastewater treatment plants are largely ineffective to remove those pollutants due to their unique chemical structures and biological toxicity of these complex compounds (Li & Yang, 2018). The traditional effluent treatment systems have insufficient removal efficiencies, and even some antibiotics proven to be toxic to

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microorganisms may be present as residue (Patel *et al.*, 2020; Verlicchi *et al.*, 2012; Krzemiński *et al.*, 2018). This insufficiency of the treatment system results in the excessive release of drug residues into the surface water, soil, and groundwater (Tahraoui *et al.*, 2022). These contaminations are accompanied by serious risks, such as toxicity, carcinogenicity, as well as bioaccumulation in the ecosystem (Aziz *et al.*, 2025). The spread of the antibiotic resistant pathogenic microbes poses a threat to the global health condition (Oluwole *et al.*, 2020). The active pharmaceutical substances and other diverse pollutants frequently require a complex treatment strategy (Shah & Shah, 2020). Therefore, an urgent and critical need created for a effective advanced treatment technologies which will be capable to mitigate the environmental impact of pharmaceutical discharges (Iyer *et al.*, 2025; Kato & Kansha, 2024).

The studied Effluent Treatment Plant (ETP) was designed to treat approximately 1.5 cubic meters of wastewater per hour. The source of liquid discharge was various pharmaceutical production units within the factory. It is important to note that effluent originating from the antibiotic units were discharged to the ETP, following a pretreatment system as per the standard protocol established by the company.

The present research seeks to present an overview and comparative analysis of several physicochemical, and biological-based processes that are used to treat pharmaceutical wastewater. This study investigates the performance of a multi-stage effluent treatment plant in Bangladesh, specifically focusing on its efficacy in removing various organic pollutants from wastewater to achieve effluent discharge standard of Department of Environment (DoE) set guideline.

2. Materials and Methods

2.1 Materials

The study was conducted over a consecutive three-month period of time (from December, 2021 to February 2022) in a pharmaceutical industry situated at Comilla district, Bangladesh. Wastewater samples were collected periodically from all treatment units of the effluent treatment plant (ETP) of the factory.

The effluent treatment system of the study plant is sequenced with equalization, pH adjustment, anaerobic followed by aerobic biodegradation, plane sedimentation followed by chemical sedimentation, reed bed bioaccumulation and post aeration. The equalization tank of the effluent treatment plant (ETP) served as the primary treatment unit, receives effluent continuously throughout the day. To maintain the optimal pH level, an automated pH adjustment system had been integrated into the equalization tank. A two-stage biological treatment process, started with the up-flow anaerobic sludge blanket (UASB) system and followed by the activated sludge process were employed. Initially, the effluent from the equalization tank is pumped into the Bioreactor-1, where anaerobic biodegradation takes place through the UASB process. Next, the partially treated effluent is discharged to Bioreactor-2, where further biodegradation of excess organic matter

occurs with Activated Sludge Process (ASP). To clarify the effluent of Bioreactor-2, a plane sedimentation system was employed with Clarifier-1. The settled sludge is then partially returned to Bioreactor-2 to maintain the desired concentration of biomass in the reactor.

The supernatant of Clarifier-1 is passed to Clarifier-2 to remove any remaining unsettled colloidal particles using a chemical sedimentation system i.e. coagulation and flocculation. Any excess sludge from Clarifier-1 and all sludge from Clarifier-2 are discharged into the Sludge Drying Bed. Finally, the sludge is disposed as solid waste after proper dewatering. The clarified effluent from the Clarifier-2 is spread over the Reed Bed followed by a Post Aeration system for polishing with combined physical and biological processes. This comprehensive multi-stage treatment approach ensures maximal removal efficiencies of pharmaceutical compounds, thereby mitigating their environmental impacts and safeguard to the public health.

The Up-flow Anaerobic Sludge Blanket (UASB) system was designed considering Organic Loading Rate (OLR) = 4 – 5 kg COD/m³-day, Hydraulic Retention Time (HRT) = 12 hours, Sludge Retention Time (SRT) = 60 days. The Activated Sludge Process (ASP) was designed considering Hydraulic Retention Time (HRT) = 12 hours, Sludge Retention Time (SRT) = 12 – 13 days, food and microorganism ratio F/M = 0.33 and oxygen requirement = 25 – 30 kg/day. Dissolved Oxygen (DO) concentration was maintained 24 hours 2 – 4 mg/l in the Bioreactor-2 for the survival of the aerobic bacteria. Coagulant and flocculent doses were fixed periodically (at least once in a week) by Jar Test in the chemical sedimentation system. PAC (Polyaluminium Chloride) and PAM (Polyacrylamide) were used as coagulant and flocculent at the dosing rate of 40 to 70 mg/l and 1 to 2 mg/l respectively.

2.2 Methodology

Water sample collection, transportation, preservation, and laboratory analysis was conducted with the Standard Method (APHA, 2017; Jenkins, 1982). All tests were conducted in the Environmental Engineering Laboratory of IUBAT, with the exception of dissolved oxygen and pH, which were performed on-site.

Samples were collected in every two weeks' interval. Three samples from each of the treatment units were collected for laboratory test. The sample were collected from the outlet portion the treatment units except for Bioractor-2. To evaluate the performance of Bioreactor-2, the clarified sample was collected from the outlet of Clarifier-1 but, to analyze MLSS and SVI sample was collected from the Bioractor-2. After field and laboratory test the concurrent result from the three samples of the same unit were recorded in the data sheet. One-liter size HDPE bottles were used to collect sample from the Bioreactor-2 for MLSS and SVI tests and 500 ml size HDPE bottles were used for the samples from other units. Sample were carried with ice box to maintain temperate below 4°C.

The studied pharmaceutical industry pre-treats the antibiotic contaminated effluent before discharging to the ETP. Alkaline hydrolysis with sodium hydroxide solution followed by neutralization with hydrochloric acid process were used to disintegrate the antibiotic molecules. In high pH (10–13) antibiotic molecules lose structural integrity and antimicrobial activity and the complex molecules convert into smaller, more biodegradable compounds.

The key effluent quality indicators (KEQI) were assessed in different treatment units of the effluent treatment plant (ETP). The tested water quality parameters are like pH, turbidity, total dissolved solids (TDS), total suspended solids (TSS), total solids (TS), mixed liquor suspended solids (MLSS), chemical oxygen demand (COD), biochemical oxygen demand (BOD₅) and sludge volume index (SVI). Each of the parameters were meticulously measured and analyzed to evaluate the performance and effectiveness of the treatment process at various treatment stages within the ETP. The status of the overall effluent treatment efficiency of different units of the treatment system are mentioned in Table 1.

Table 1. Effluent Parameters Tested in Different Units.

Unit No	Name of the Treatment Unit	Effluent Parameters
1	Equalization Tank (Eqn. T)	pH, Turbidity, TDS, TSS, TS, BOD ₅ and COD
2	Bioreactor-1 (BR-1)	pH, Turbidity, TDS, TSS, TS, BOD ₅ and COD
3	Bioreactor-2 (BR-2)	pH, Turbidity, TDS, MLSS, TS and SVI
4	Clarifier-1 (Clr-1)	pH, Turbidity, TDS, TSS, TS, BOD ₅ and COD
5	Clarifier-2 (Clr-2)	pH, Turbidity, TDS, TSS, TS, BOD ₅ and COD
6	Reed Bed (RB)	pH, Turbidity, TDS, TSS, TS, BOD ₅ and COD
7	Post Aeration Tank (PAT)	pH, Turbidity, TDS, TSS, TS, BOD ₅ and COD

During the three months' research period, effluent quality data were collected in five times from all the units of the ETP. The obtained data from different treatment units were accumulated and prepared for statistical analysis using Microsoft Excel and finally the relevant inferences were drawn. The comprehensive dataset generated a robust evaluation approach of the multi-stage treatment system based ETP.

3. Results and Discussion

The laboratory test results which had been found during the study period from the different treatment units of the ETP are summarized and compared with DoE effluent discharge standards (ECR 2023). The summary of the ANOVA result is shown in Table 2. The laboratory test results with mean and standard deviation (SD) is show in Table 3.1 and Table 3.2. The results show the variation of pollution removal efficiencies of different units. Some significant variations observed in individual processes as well. Several key effluent quality indicators (KEQI) reflect the performance of these treatment units. Based on the characteristics of the effluent and the treatment process, Turbidity, TDS, TSS, COD, and BOD₅ are considered as the KEQI for evaluating the ETP.

Table 2: ANOVA Results Summary

Parameter	F-value	p-value	Statistical Interpretation
pH	6.61	< 0.001	Significant
Turbidity	112.40	< 0.001	Highly significant
TDS	3.58	0.009	Significant
TSS	38.57	< 0.001	Highly significant
TS	38.00	< 0.001	Highly significant
COD	85.25	< 0.001	Highly significant
BOD ₅	146.72	< 0.001	Highly significant

pH: The value of pH remains within the limit of effluent discharge standard under all treatment steps. It fluctuated little bit in different chemical and biological treatment units. A statistically significant difference in pH ($F = 6.61$, $p < 0.001$) is show among treatment units by the One-way ANOVA test.

Turbidity: The turbidity of influent water was found as 201 ± 101 FTU, primarily attributed to colloidal pharmaceutical particles. The turbidity of effluent had been significantly and progressively decreased through various treatment stages. Turbidity showed a highly significant difference among treatment units ($F = 112.40$, $p < 0.001$), indicating effective clarification and polishing through downstream units. A significant reduction was observed after aerobic biodegradation in Bioreactor-2 followed by clarification. Chemical coagulation, flocculation, and subsequent clarification proven effective in removing most of the turbidity caused by colloidal particles present in the effluent. Additionally, a reed bed system also played a significant role in removal of turbidity. Ultimately, the discharged effluent became turbidity free. This study demonstrates the efficacy of

the multi-stage treatment process to achieve a high degree of clarity to meet the environmental discharge standard. A system based on various treatment processes, including sedimentation, filtration, and plant uptake, can achieve substantial reductions in suspended solids and associated turbidity (Pastor-López *et al.*, 2024). The final effluent from pharmaceutical effluent treatment plants should have an aim to achieve a turbidity of less than 5 NTU (Jegatheesan *et al.*, 2022). The Nephelometric Turbidity Units (NTU) are considered comparable to the Formazin Turbidity Units (FTU) when turbidity is measured by nephelometry calibrated with a formazin standard reference suspension (US EPA Method 180.1). The integrated physical, chemical, and biological processes of the treatment system ensures such removal efficiency of turbidity (Wondim *et al.*, 2023).

TDS: The treatment system could not remove dissolved solids from the effluent at all. On the contrary, after chemical treatment, due to the addition of coagulant and flocculent, TDS increased from 400 ± 33 mg/l to 522 ± 75 mg/l. A statistically significant variation in TDS was observed across treatment units ($F = 3.58$, $p < 0.01$), although the magnitude of change was comparatively low. This observation proves that the chemical treatment methods can elevate the total dissolved solids concentration in the treated water (Makowska *et al.*, 2023). In some cases advanced treatment methods may be required to effectively manage TDS levels before final discharge (Abdelfattah *et al.*, 2022).

TSS: The concentration of total suspended solids differed highly significantly among treatment units ($F = 38.57$, $p < 0.001$), confirming efficient suspended solids removal. The suspended solid concentration in the ETP influent was found as 512 ± 272 mg/l. The TSS concentration had been slightly decreed in the discharged effluent from Bioreactor-1. Further, a massive increase occurred in Bioreactor-2, due to the presence of biomass in the aeration tank. The suspended solids in the aeration tank, referred to as mixed liquor suspended solids (MLSS), reached a concentration of 4346 ± 1481 mg/l. Such MLSS value indicates presence of a substantial and active microbial biomass in the reactor. This is crucial for the biological degradation of complex pollutants in pharmaceutical wastewater (Bermúdez *et al.*, 2023; Govindaraju *et al.*, 2022). The concentration of suspended solids decreased abruptly after both the physical and chemical clarification systems. At the final effluent discharge point TSS concentration reduced to 13 ± 6 mg/l. Both physical and chemical treatments are highly effective in reducing TSS to the acceptable discharge levels. The physicochemical process, including coagulation, flocculation, sedimentation, clarification, and various filtration techniques are crucial for suspended solids removal (Chhetri *et al.*, 2016; Konring & Tang, 2016). These physicochemical processes separate colloidal and suspended particles from the effluent and ensure the environmental discharge standards (Konring & Tang, 2016; Ponce-Robles *et al.*, 2022). The multi-stage treatment technique, combination of biological with physical and chemical separation, can effectively remove complex particulate matter in pharmaceutical effluent also (Konring & Tang, 2016; Ponce-Robles *et al.*, 2022).

Both from the field and laboratory test, the sludge from Bioreactor-2 was observed as compact nature. The average sludge volume index from the sample was found as $58 \pm 13 \text{ ml/g}$. An SVI value below 100 ml/g indicates good settling characteristics and that type sludge settles well in the clarifier without bulking (Khudhair *et al.*, 2023; Rashid, 2024). This efficient settling characteristic of sludge ensured clearer effluent with simple solid-liquid separation system.

Table 3.1: The Effluent Test Results of Different Treatment Units and DoE Standard

Sapling Units	pH			Turbidity (FTU)			TDS (mg/l)			TSS (mg/l)		
	Value	Mean	SD	Value	Mean	SD	Value	Mean	SD	Value	Mean	SD
Eqn. T	6.76	6.48	0.42	298	201	101	410	400	33	60	512	272
Eqn. T	7.08			92			350			670		
Eqn. T	6.12			288			410			640		
Eqn. T	6.28			233			440			730		
Eqn. T	6.18			95			390			460		
BR-1	6.18	6.28	0.21	164	199	94	480	398	76	320	480	136
BR-1	6.58			350			330			620		
BR-1	6.39			188			310			610		
BR-1	6.02			199			460			480		
BR-1	6.21			92			410			370		
BR-2	6.73	7.03	0.65	31	53	34	510	436	65	5340	4346	1481
BR-2	6.62			37			390			6260		
BR-2	6.43			112			350			4040		
BR-2	7.41			53			470			2480		
BR-2	7.98			32			460			3610		
Clr-1	7.05	7.20	0.52	64	47	29	500	410	82	140	68	50

Clr-1	6.72			64			350			40		
Clr-1	6.82			40			300			20		
Clr-1	7.40			69			450			100		
Clr-1	7.99			0			450			40		
Clr-2	5.74	6.33	0.54	0.55	0.49	0.17	620	518	78	50	26	15
Clr-2	6.09			0.48			520			20		
Clr-2	6.03			0.42			400			30		
Clr-2	6.82			0.74			520			20		
Clr-1	6.98			0.28			530			10		
RB	6.62	6.99	0.43	0.45	0.09	0.20	630	522	75	15	20	12
RB	6.93			0			520			10		
RB	6.6			0			420			35		
RB	7.2			0			510			30		
RB	7.62			0			530			10		
PAT	7.35	7.78	0.43	0	0.00	0.00	630	522	75	20	13	5
PAT	7.58			0			520			10		
PAT	7.52			0			420			17		
PAT	8.07			0			510			10		
PAT	8.38			0			530			10		
DOE Standard	6.0 – 9.0			-			≤ 2100			≤ 100		

Table 3.2: The Effluent Test Results of Different Treatment Units and DoE Standard

Sapling	TS (mg/l)	COD (mg/l)	BOD5 (mg/l)	SVI (ml/g)
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Units	Value	Mean	SD	Value	Mean	SD	Value	Mean	SD	Value	Mean	SD
Eqn. T	470	912	272	1378	2034	441	788	1126	224			
Eqn. T	1020			2014			1128					
Eqn. T	1050			2326			1230					
Eqn. T	1170			1918			1086					
Eqn. T	850			2532			1398					
BR-1	800	878	81	1368	1691	275	417	708	245			
BR-1	950			1414			860					
BR-1	920			1928			916					
BR-1	940			1874			880					
BR-1	780			1872			465					
BR-2	5850	4782	1470	323	219	76	65	94	23	36	58	13
BR-2	6650			114			81			69		
BR-2	4390			224			127			59		
BR-2	2950			241			98			59		
BR-2	4070			193			101			69		
Clr-1	640	478	127	284	238	97	162	99	62			
Clr-1	390			162			70					
Clr-1	320			167			53					
Clr-1	550			387			171					
Clr-1	490			192			41					
Clr-2	670	544	85	183	145	36	74	40	20			

Clr-2	540			124			33					
Clr-2	430			134			28					
Clr-2	540			183			38					
Clr-1	540			103			27					
RB	645	542	68	140	104	23	58	35	14			
RB	530			108			36					
RB	455			104			25					
RB	540			82			33					
RB	540			88			25					
PAT	650	535	76	129	99	30	41	29	7			
PAT	530			109			29					
PAT	437			94			21					
PAT	520			51			27					
PAT	540			114			28					
DOE Standard	-			≤ 200		≤ 30			-			

COD: The concentration of COD decreased significantly along the treatment train ($F = 85.25$, $p < 0.001$), demonstrating strong organic matter removal efficiency. The concentration of chemical oxygen demand in the influent was found as 2034 ± 441 mg/l. The COD concentration of raw effluent shows presence of a typical organic load in wastewater (Makowska *et al.*, 2023). A remarkable reduction of COD occurred in the Bioreactor-1, where it decreased to 1691 ± 275 mg/l through anaerobic biodegradation. Such COD reduction signifying the initial efficacy of the UASB system by metabolizing readily biodegradable organic compounds as other studied also found (Bazedi *et al.*, 2023). This reduction was more significantly enhanced after treatment in Bioreactor-2, in an aerobic biological stage. The subsequent clarification, leading to a substantial decrease in COD to 238 ± 97 mg/l. This treatment stage effectively removes biodegradable organic pollutants through aerobic microbial degradation and removes associated suspended solids via clarification (Chalaris *et al.*, 2023; Shtepa *et al.*, 2021). Bacterial treatment processes have demonstrated significant

COD reductions, with some studies reporting reductions to 134 ± 0.74 mg/l from initial values of 2035 ± 0.61 mg/l (Bhargawa *et al.*, 2024).

The additional COD value reduction observed following chemical clarification and it decreased to 145 ± 36 mg/l. This physicochemical process plays a crucial complementary role by removing residual organic matter, including colloidal particles and recalcitrant pharmaceutical substances that often present after biological treatment (Guo *et al.*, 2017; Malik *et al.*, 2019; Patel *et al.*, 2020). The sequential application of biological and chemical treatments process is essential for effectively removing the complex, recalcitrant and often low-biodegradable organic elements of pharmaceutical effluents (Khalidi-Idrissi *et al.*, 2023; Malik *et al.*, 2019). The Reed Bed and Post Aeration system also removed some amount of COD. The final concentration of COD at the outlet of the Post Aeration Tank was measured as 99 ± 30 mg/l. Other studies have demonstrated that various phytoremediation agents can reduce COD ranging from 52% to 91% and up to 99% using combined physicochemical and biochemical techniques (Fitrisyaah *et al.*, 2025; Bazedi *et al.*, 2023).

BOD: The biochemical oxygen demand reduction pattern of the effluent was similar to those observed for COD. The reduction of BOD₅ showed the highest statistical significance among all parameters ($F = 146.72$, $p < 0.001$), highlighting the effectiveness of biological treatment processes. The BOD₅ of influent was initially measured as 1126 ± 224 mg/l. This concentration successively decreased to 708 ± 245 mg/l in Bioreactor-1, then to 99 ± 62 mg/l after Bioreactor-2 and subsequent clarification, and further to 40 ± 20 mg/l following chemical clarification. A slight reduction was also observed after passing through Reed Bed, culminating in a final BOD₅ concentration of 29 ± 7 mg/l at the Post Aeration Tank discharge point. The overall BOD reduction scenario demonstrates the effectiveness of the integrated treatment system to mitigate the pollution and ensures the effluent quality within acceptable limits for discharge. The various pre-treatment methods, such as chemical oxidants like hydrogen peroxide, Fenton's reagent, potassium persulfate etc. can significantly improve biodegradability of pharmaceutical compounds (Iyer *et al.*, 2025). Different Biological processes, particularly bacterial treatment or plant-based systems, have demonstrated substantial efficiency in reducing biochemical oxygen demand and chemical oxygen demand in pharmaceutical wastewater (Bazedi *et al.*, 2023; Bhargawa *et al.*, 2024; Pandya *et al.*, 2022).

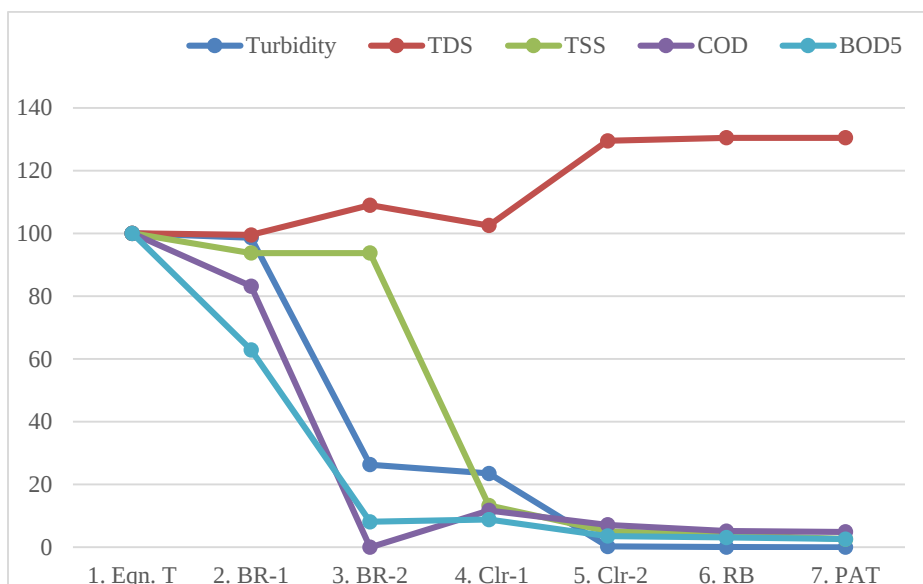


Figure 1: Percentile Pollution Removal Efficiency Curve of Different Units

The Figure-1 demonstrates the gradual removal of pollutants during the treatment process. Most pollutants were effectively removed except TDS at the 5th stage of treatment in Clarifier-2. At the final treatment stage, the water achieved complete removal of turbidity, 97% removal of TSS, 95% of COD, and 97% of BOD₅ from the raw influent. Though 31% increment of TDS after the end process, its final concentration remained within acceptable limits.

The Figure 2 highlights the notable improvements in wastewater treatment achieved by the individual treatment units. Utilizing the UASB technique in Bioreactor-1, it was achieved reductions of 17% in COD and 37% in BOD₅. The Clarifier-1, employing the activated sludge process had achieved 86% removal of TSS, COD, and BOD₅. Turbidity removal efficiency found in Clarifier-1 as 76%, while Clarifier-2 exceeded the expectations with a remarkable efficiency of 99%. The Clarifier-2 also showed pollution removal efficiencies of 62%, 39%, and 60% for TSS, COD, and BOD₅ respectively. The Reed Bed unit had shown its pollution removing effectiveness by 82% turbidity, 23% TSS, 28% COD, and 12% BOD load. No turbidity was found in the post aeration unit, i.e. 100% turbidity removed; other parameters like TSS, COD and BOD was removed 33%, 5% and 17% respectively.

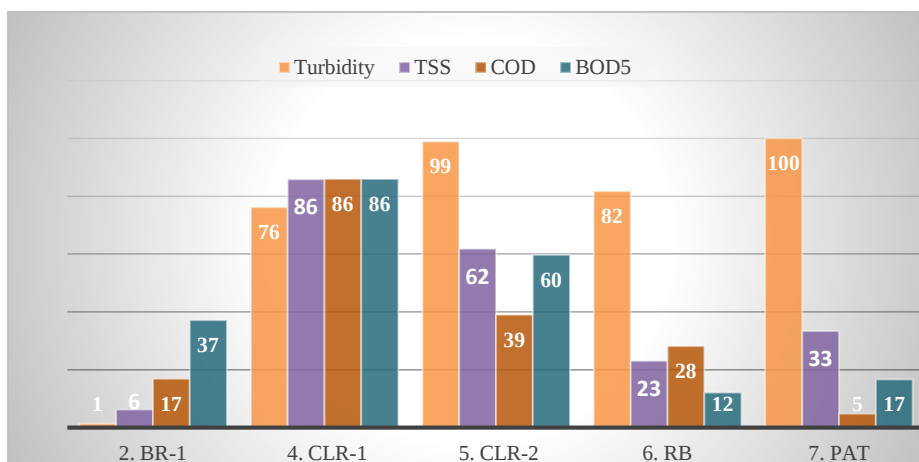


Figure 2: Percentile Pollution Removal Efficiency of Individual Treatment Units

During the study, it was observed that Bioreactor-1 removed 343 mg/l of COD. Assuming the plant operation period of 20 hours per day at a flow rate of 1.5 m³/hr; the biogas generation rate can be calculated, as mentioned by Tchobanoglous *et al.*, 2003 and He *et al.*, 2019. Specific operational parameters and wastewater characteristics must be kept in account for the calculations predicted biogas yield. The following equation derived at a temperature of 25°C:

$$\begin{aligned}
 \text{Methane Production Rate} &= \text{COD (g/m}^3\text{)}/\text{day} \times 382 \times 10^{-6} \\
 &= \text{m}^3/\text{day} \\
 &= 1.5 \times 20 \times 343 \times 382 \times 10^{-6} \text{ m}^3/\text{day} \\
 &= 3.93 \text{ m}^3/\text{day}
 \end{aligned}$$

A study by (Dai *et al.*, 2019) reported that 1 gram of COD can generate approximately 16.1 kilo-joules of energy. Therefore, the estimated energy production potential of the studied ETP is approximately 166 mega-joules per day. Such integration of treatment system can lead to a new approach of energy savings and some extent of energy neutrality (Dai *et al.*, 2019).

The studied effluent treatment plant meets the discharge quality standards as per the regulations of Environmental Conservation Rules (ECR, 2023). The extent of removal efficiency varies significantly depending on the specific pharmaceutical compounds and the operational efficiency of each treatment unit (Akinwumi *et al.*, 2023). These advanced treatment approaches open an avenue toward more effective elimination of recalcitrant pharmaceutical contaminants from the wastewater streams (Twi-Yeboah *et al.*, 2024).

5. Conclusion

Three months' examination of the effluent treatment plant revealed that the end result of the discharge of the effluent met all the necessary parameters as guided

by the department of Environment. In case of COD and BODs removal extremely high F-values confirm biological treatment as the dominant removal mechanism. The significant improvements of TSS, TS, and turbidity removal reflect effectiveness of clarification and reed bed filtration system. The TDS value in the effluent was lower but not efficiently removed by conventional biological treatment system. The statistically significant differences of the pH are operationally acceptable and do not hinder treatment performance. The Water quality results shows that Bioreactor-2 was more effective in removing organic pollutants compared to Bioreactor-1. The aerobic treatment shown better results than anaerobic treatment with the same detention time in removing organic pharmaceutical pollutants. In case of sedimentation, chemical sedimentation process was found more effective compared to plane sedimentation in terms of eliminating BOD, COD, and TSS. But, the level of TDS significantly increased in the course of chemical treatment. Reed Bed system was found mainly effective in the removal of turbidity and suspended solids. The varying physicochemical characteristics of pharmaceutical compounds require different treatment methods. Pollution removal efficiencies of pharmaceutical effluent may vary dramatically even within the same therapeutic group, based on aspects such as biomass concentration, hydraulic retention time, and pH. Treatment of pharmaceutical effluent with biological treatment is usually necessary to obtain complete elimination of all recalcitrant chemicals and to obtain desirable discharge limits.

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Conflict of interest

The authors declare no potential conflict of interest regarding the publication of this work. In addition, the ethical issues including plagiarism, informed consent, misconduct, data fabrication and, or falsification, multiple publication and, or submission, and redundancy have been completely witnessed by the authors.

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